

## TITLE OF THE INVENTION

### **COMPACT SELF-BALLASTED FLUORESCENT LAMP WITH IMPROVED RISING CHARACTERISTICS**

5           This application is based on application No. 2003-55003  
filed in Japan, the contents of which are hereby incorporated  
by reference.

## BACKGROUND OF THE INVENTION

### 10   (1) Field of the Invention

          The present invention relates to a compact  
self-ballasted fluorescent lamp including an arc tube composed  
of a glass tube at least partially bent and electrodes with  
filament coils sealed at both ends of the glass tube, and  
15   a holder having insertion openings and holding the arc tube  
by fixing the ends of the glass tube inserted through the  
insertion openings.

### (2) Related Art

20           In the present energy-saving era, compact  
self-ballasted fluorescent lamps have been increasingly  
widespread as energy-saving light sources alternative to  
incandescent lamps. As one example, a compact self-ballasted  
fluorescent lamp includes an arc tube formed by winding a  
25   glass tube in a double-spiral shape and enclosing mercury  
in the glass tube, a holder holding the arc tube, an electronic

ballast contained in the holder for lighting the arc tube, a globe covering the arc tube, and a screw-type base attached to the holder.

At both ends of the glass tube, electrodes with filament  
5 coils are sealed. The holder has a pair of insertion openings through which the ends of the glass tube are inserted in the holder. Some compact self-ballasted fluorescent lamps have such a construction where the arc tube is held by the holder in a state where the filament coils placed in the glass tube  
10 are positioned within the holder (see Japanese Laid-Open Patent Application No. H8-339780). To efficiently obtain visible light emitted from the arc tube, however, compact self-ballasted fluorescent lamps having such a construction where the filament coils are positioned outside the holder  
15 have been developed in recent years.

Compact self-ballasted fluorescent lamps with the construction where the filament coils are positioned outside the holder can feature an improved amount of light emission. After the cumulative lighting time of long hours, however,  
20 these lamps start to suffer from poor rising characteristics at the lighting startup compared with the initial stage of their use.

FIG. 1 shows the relationship between a relative luminous flux value and an elapsed lighting time for a conventional  
25 compact self-ballasted fluorescent lamp. The relative

luminous flux value is a luminous flux value relative to a  
luminous flux value during the steady lighting state, at the  
lighting startup of the conventional compact self-ballasted  
fluorescent lamp. Here, the conventional compact  
5 self-ballasted fluorescent lamp is repeatedly made ON and  
OFF with its base being oriented upward, until a total lighting  
time reaches 100 hours and 6000 hours. The total lighting  
time is a total of ON times when a ON/OFF cycle of "two hours  
and 45 minutes ON" and "15 minutes OFF" is repeated.

10 As shown in the figure, for the conventional compact  
self-ballasted fluorescent lamp, the time required by the  
relative luminous flux value during the steady lighting state  
to reach 60% is about 7.5 seconds for the total lighting time  
of 100 hours, whereas the time is about 20.5 seconds for the  
15 total lighting time of 6000 hours. The time required by the  
relative luminous flux value to reach 60% for the total lighting  
time of 6000 hours is 2.7 times as long as that for the total  
lighting time of 100 hours. In this way, after the total  
lighting time of long hours, the lamp starts to suffer from  
20 poor rising characteristics at the lighting startup compared  
with the initial stage of its use.

#### SUMMARY OF THE INVENTION

In view of the above problem, the object of the present  
25 invention is to provide a compact self-ballasted fluorescent

lamp with improved rising characteristics at the lighting startup after the cumulative lighting time of long hours while maintaining the emitted luminous flux.

The above object of the present invention can be achieved  
5 by a compact self-ballasted fluorescent lamp, including: an arc tube including a glass tube at least partially bent, and electrodes sealed at both ends of the glass tube, each electrode including a filament coil; and a holder having a pair of insertion openings formed therein, and holding the  
10 arc tube by fixing the ends of the glass tube inserted through the insertion openings, wherein the ends of the glass tube are inserted to such positions that enable each filament coil to be positioned within the holder, and a minimum distance  $L_1$ , in an insertion direction of the ends of the glass tube,  
15 between each filament coil and an edge of corresponding one of the insertion openings is in a range of 0 to 10 mm inclusive.

According to this construction, the temperature at positions on the glass tube in the vicinity of the filament coils can be raised while the lamp can maintain substantially  
20 the same luminous flux as the luminous flux of conventional lamps. Accordingly, concentration of mercury in the vicinity of the filament coils can be suppressed, thereby preventing the amount of mercury present within the glass tube from being reduced. Due to this, even after the total lighting time of  
25 long hours, the lamp can have improved rising characteristics

at the lighting startup.

#### BRIEF DESCRIPTION OF THE DRAWINGS

These and other objects, advantages and features of the  
5 invention will become apparent from the following description  
thereof taken in conjunction with the accompanying drawings  
that illustrate a specific embodiment of the invention.

In the drawings:

FIG. 1 is a graph showing rising characteristics of a  
10 conventional compact self-ballasted fluorescent lamp at the  
lighting startup;

FIG. 2 is a front view of a compact self-ballasted  
fluorescent lamp relating to a preferred embodiment of the  
present invention, with being partially cut away;

15 FIG. 3 is a front view of an arc tube relating to the  
embodiment of the present invention, with being partially  
cut away;

FIG. 4A is a plan view of a holding member relating to  
the embodiment of the present invention;

20 FIG. 4B is a side view of the holding member relating  
to the embodiment of the present invention;

FIG. 5 is a front view of the arc tube held by the holding  
member relating to the embodiment of the present invention;

FIG. 6 is an enlarged view of an end-vicinity part of  
25 a glass tube inserted in the holding member relating to the

embodiment of the present invention;

FIG. 7 is a graph showing rising characteristics of the compact self-ballasted fluorescent lamp relating to the embodiment of the present invention at the lighting startup;

5        FIG. 8A is a front view of a compact self-ballasted fluorescent lamp relating to a modification of the present invention, with being partially cut away;

FIG. 8B is an enlarged sectional view of "A" part shown in FIG. 8A; and

10        FIG. 9 is a front view of a fluorescent lamp to which the present invention is applied.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

The following describes a compact self-ballasted  
15        fluorescent lamp relating to a preferred embodiment of the present invention, with reference to FIGS. 2 to 7.

##### 1. Construction

##### (a) Overall Construction

As shown in FIG. 2, a compact self-ballasted fluorescent  
20        lamp 100 relating to the present embodiment includes an arc tube 110 formed by a glass tube 120 wound into a double-spiral shape, a holder 200 holding the arc tube 110, an electronic ballast 300 contained in the holder 200 for lighting the arc tube 110, and a globe 400 covering the arc tube 110.

25        The electronic ballast 300 employs a series-inverter

method, and includes a plurality of electric components such as capacitors 310, 330, 340, and a choke coil 320. These electric components of the electronic ballast 300 are mounted on a substrate 360, which is attached to a holding member  
5 210 described later.

The holder 200 includes the holding member 210 with a cylindrical shape having a closed bottom, and a case 250 that is fit to cover a circumferential wall of the holding member 210. The case 250 has a cone shape, and includes a cylindrical  
10 part with a larger opening (hereafter referred to as a large-diameter cylindrical part) 251, and a cylindrical part with a smaller opening (hereafter referred to as a small-diameter cylindrical part) 252. The large-diameter cylindrical part 251 is fit to cover the circumferential wall  
15 220 of the holding member 210. To the small-diameter cylindrical part 252, the base 380 is attached.

As in the case of a globe used in incandescent lamps, the globe 400 is made from a glass material that can have a beautiful finish in its design, and is in the "A" shape.  
20 It should be noted here that the shape of the globe 400 should not be limited to the "A" shape.

The globe 400 is attached to the holding member 210 and the case 250 by placing its open end 405 between the circumferential wall 220 of the holding member 210 and the  
25 large-diameter cylindrical part 251 of the case 250 that is

fit to cover the circumferential wall 220 of the holding member 210. The globe 400 is bonded via a bonding agent 420 filled between the holding member 210 and the case 250.

The inner surface of a top part 406 of the globe 400 is thermally connected to a projected part 126 formed at the top of the arc tube 110 via a heat-conductive medium 410, specifically, silicone resin.

#### (b) Arc Tube

As shown in FIG. 3, the arc tube 110 has a double-spiral shape, and includes a turning unit 121 formed by turning the glass tube 120 at its middle, and two spiral units 122 and 123 formed by spirally winding glass tube parts that extend from the turning unit 121 to both ends 124 and 125 of the glass tube 120, in the B direction (this direction may be hereafter referred to as the "spiral direction") around the axis A of spiral (spiral axis A). It should be noted here that the ends 124 and 125 of the glass tube 120 referred to in this specification intend to mean the very edges of both ends of the glass tube 120. It should be noted here that the direction parallel to the spiral axis A is hereafter referred to as the "spiral-axis direction".

The glass tube 120 (specifically, each of the spiral units 122 and 123) is wound with substantially the same pitch, i.e., a first pitch, from its middle (corresponding to the turning unit 121) to a predetermined position (hereafter



referred to as a "pitch enlarging position"), and with a second pitch larger than the first pitch from the pitch enlarging position to the ends 124 and 125 of the glass tube 120 (the parts of the glass tube 120 from the pitch enlarging position to the ends 124 and 125 may be hereafter referred to as "end-vicinity parts"). Due to the second pitch, the ends 124 and 125 are away from glass tube parts that are adjacent to the ends 124 and 125 in the spiral-axis direction. A "pitch" referred to herein is "Plt" in FIG. 3, and is specifically a distance between the central points of the cross sections of two glass tube parts adjacent to each other in the spiral-axis direction.

To be more specific, the glass tube 120 is wound at an inclination angle  $\alpha$  with respect to the spiral axis A (hereafter referred to as the "spiral angle"), from its middle (corresponding to the turning unit 121) to the pitch enlarging position, and at an inclination angle  $\beta$  smaller than the inclination angle  $\alpha$  with respect to the spiral axis A from the pitch enlarging position to the ends 124 and 125.

It should be noted here that soft glass such as strontium-barium silicate glass is used as a material for the glass tube 120.

Electrodes 130 are sealed at the ends 124 and 125 of the glass tube 120. The electrodes 130 each are composed of a filament coil 131 and a pair of lead wires 133 and 134

supporting the filament coil 131 by a bead glass mounting method. The filament coils 131 are made of tungsten formed into a triple spiral shape, and an amount of for example 2 mg of an electron emissive material mainly composed of BaO-CaO-SrO is filled thereon. The electrodes 130 are sealed in such a manner that the filament coils 131 are inserted into the glass tube 120 to such positions away by a predetermined distance from the ends 124 and 125.

An exhaust tube 140 is sealed, together with the electrode 130, at one of the ends 124 and 125 of the glass tube 120, i.e., the end 124, to exhaust the glass tube 120 to create a vacuum therein or to enclose mercury, a buffer gas, or the like therein described later. The tip of the exhaust tube 140 is sealed for example by tip-off, after the glass tube 120 is exhausted and mercury and a buffer gas are enclosed.

Within the glass tube 120, about  $3 \pm 0.3$  mg of mercury, and argon as a buffer gas are enclosed at a pressure of 600 Pa. As the buffer gas, a mixture gas such as a mixture of argon and neon may also be used.

Mercury is enclosed in the glass tube 120 in such form that can exhibit a mercury vapor pressure value during lighting of the arc tube 110 equivalent to a mercury vapor pressure value exhibited by mercury that is substantially singly enclosed. To be more specific, mercury is enclosed in the

form of tin mercury (Sn-Hg) 151 that can exhibit a mercury vapor pressure value during lighting close to a mercury vapor pressure value exhibited by substantially single mercury.

It should be noted here that mercury, for example, an alloy of mercury and tin, enclosed in the glass tube 120 is referred to as "mercury in substantially single form" as long as the mercury has substantially the same action as singly enclosed mercury.

As the tin mercury 151, an alloy of 80 wt% tin and 20 wt% mercury is used. It should be noted here that the mercury exhibiting a mercury vapor pressure value equivalent to a mercury vapor pressure value exhibited by mercury in substantially single form during lighting of the arc tube 110 may be zinc mercury (Zn-Hg), in addition to tin mercury mentioned above.

A phosphor 150 is applied to the inner surface of the glass tube 120. The phosphor 150 used here may be a mixture of three types of rare-earth phosphors respectively emitting red, green, and blue light, e.g.,  $Y_2O_3:Eu$ ,  $LaPO_4:Ce$ , Tb, and  $BaMg_2Al_{16}O_{27}:Eu$ , Mn.

#### (c) Holder

As shown in FIGS. 2, 4A, and 4B, the holding member 210 is roughly composed of an end wall 230 and a circumferential wall 220. As one example, PET (polyethylene terephthalate) is used as a material for the holding member 210. This resin

has good heat-resistant properties, and also has strong resistance to ultraviolet rays.

The following first describes the end wall 230. The end wall 230 has a pair of insertion openings 231 and 232 through which the ends 124 and 125 of the glass tube 120 are inserted into the holding member 210, a pair of guide units 233 and 234 for guiding the ends 124 and 125 of the glass tube 120 to the insertion openings 231 and 232, and a pair of cover units 235 and 236 for covering the end-vicinity parts 124a and 125a of the inserted glass tube 120.

The insertion openings 231 and 232, the guide units 233 and 234, and the cover units 235 and 236 are formed as symmetric pairs with respect to a central point O of the end wall 230. Hereafter, the side toward which the end 124 (125) of the glass tube 120 moves in the process of inserting the glass tube 120 into the holding member 210 is referred to as the "lower side", and the side opposite to the lower side is referred to as the "upper side".

At the upper sides of the insertion openings 231 and 232, the guide units 233 and 234 are formed. The guide units 233 and 234 are formed as grooves that are recessed from the surface of the end wall 230, to have such shapes that correspond to the outer shapes of the lower portions of the end-vicinity parts 124a and 125a of the glass tube 120.

The guide units 233 and 234 come in contact with the

outer surfaces of the lower portions of the ends 124 and 125 of the glass tube 120, and guide the ends 124 and 125 to the insertion openings 231 and 232 when the arc tube 110 is rotated around the central axis of the holding member 210 in a state  
5 where the spiral axis A of the arc tube 110 matches the central axis of the holding member 210.

At the lower sides of the insertion openings 231 and 232, the cover units 235 and 236 are formed. The cover units 235 and 236 are formed as arches projecting from the surface  
10 of the end wall 230 to have such shapes that correspond to the outer shapes of the upper portions of the end-vicinity parts 124a and 125a of the glass tube 120. The arches are formed lower as being less closer to the insertion openings 231 and 232.

15 The insertion openings 231 and 232 are specifically formed by both the lower-side edges of the guide units 233 and 234 and the upper-side edges of the cover units 235 and 236. As shown in FIG. 4B, the upper-side edges of the cover units 235 and 236 are inclined toward the lower-sides with  
20 respect to the central axis of the holding member 210 as viewed from side of the holding member 210. As shown in FIG. 4A, the insertion openings 231 and 232 open as viewed from above.

The following then describes the circumferential wall 220 of the holding member 210. As shown in FIG. 2 and FIG.  
25 4B, a pair of substrate supporting units 222, a pair of substrate

engagement units 223 and 224, and a pair of contact units 221 are formed on the circumferential wall 220 of the holding member 210. The substrate supporting units 222 are for supporting the substrate 360 on which the electronic ballast 300 is mounted. The substrate engagement units 223 and 224 are to be engaged at one surface of the substrate 360 closer to the base 380. The contact units 221 are for coming in contact with the peripheral edge of the substrate 360.

On the entire peripheral edge of the opening of the circumferential wall 220 (opposite to the end wall 230), a flange unit 228 is formed to project outward. The flange unit 228 is engaged with projected parts (not shown) formed at the inner surface of the case 250, so that the holding member 210 and the case 250 are combined together.

The following describes the state where the holding member 210 with the above-described construction holds the arc tube 110. The holding member 210 holds the arc tube 110 by bonding the end-vicinity parts 124a and 125b (which may include the ends 124 and 125) of the glass tube 120 inserted through the insertion openings 231 and 232 as shown in FIG. 5 and FIG. 6, to the inner surface of the holding member 210 via silicone resin 390 or the like as shown in FIG. 2.

Here, the filament coils 131 placed in the glass tube 120 are positioned within the holding member 210. As shown in FIG. 6, the minimum distance L1 between (a) the filament

coil 131 and (b) the edge of the insertion opening 231 (232) of the holding member 120 in the direction where the end 124 (125) of the glass tube 120 is inserted (insertion direction), is set in a range of 0 to 10 mm inclusive. Here, even when  
5 the minimum distance L1 is 0 mm, i.e., when half portions of the filament coils 131 are positioned within the holding member 210, the filament coils 131 are assumed to be positioned within the holding member 210.

As shown in FIG. 6, the minimum distance L1 is a distance  
10 between a plane F1 and a plane F2 in the insertion direction D of the glass tube 120. The plane F1 is a plane that includes positions on the filament coil 131 that are supported by the lead wires 133 and 134, and that is perpendicular to the tubular axis C1 of the glass tube 120. The plane F2 is a plane that  
15 includes positions, closest to the filament coil 131 in the insertion direction D, on the boundary at which the glass tube 120 inserted through the insertion openings 231 and 232 enters in the holding member 210 (the edges of the insertion openings 231 and 232), and that is perpendicular to the tubular  
20 axis C1.

Here, the positioning of the filament coils 131 is expressed using their minimum distance L1 from the edges of the insertion openings 231 and 232 respectively, due to the following reason. The edges of the insertion openings 231  
25 and 232 are inclined with respect to the central axis of the

holding member 210 (see FIG. 4B), in such a manner that the insertion openings 231 and 232 are open as viewed from above the holding member 210 (see FIG. 4A). In this case, the distance between (a) the filament coils 131 positioned within the holding member 210 and (b) the edges of the insertion openings 231 and 232 respectively varies depending on the positions on the edges of the insertion openings 231 and 232.

## 2. Specific Constructions

The compact self-ballasted fluorescent lamp 100 relating to the present embodiment corresponds to a 60W incandescent lamp. Therefore, an arc tube having spiral units 122 and 123 wound by 4.5 winds together is used as the arc tube 110, and an E17-type base is used as the base 380.

The compact self-ballasted fluorescent lamp 100 (globe 400) has a maximum diameter D of 55 mm, and a total length L of 108 mm, which is smaller than incandescent lamps whose maximum diameter is 60 mm and total length is 110 mm.

For the lamp performances, the compact self-ballasted fluorescent lamp 100 exhibits the luminous flux of 820 lm and the luminous efficiency of 68.3 lm/W when the lamp input is 12W. In the life test, the compact self-ballasted fluorescent lamp 100 is confirmed to satisfy a targeted value of 6000 hours.

The following describes the dimensions of the arc tube 110, with reference to FIG. 3.



The arc tube 110 has an annular outer diameter  $D_a$ , i.e., a diameter of the arc tube 110 at an outermost circumference of the spirally wound glass tube 120, being 36.5 mm, a tube inner diameter  $\phi_i$  of the glass tube 120 being 7.4 mm, and  
5 a tube outer diameter  $\phi_o$  of the glass tube 120 being 9 mm. It is preferable that the annular outer diameter  $D_a$  of the arc tube 110 is in a range of 30 to 40 mm inclusive, to make the arc tube 110 substantially equal in size to incandescent lamps.

10 It is preferable that the tube outer diameter  $\phi_o$  of the glass tube 120 is smaller than 10 mm. This is due to the following reason. When the tube outer diameter  $\phi_o$  is 10 mm or larger, the glass tube 120 has large flexural rigidity, and therefore, it is difficult to spirally wind the glass  
15 tube 120 to have the annular outer diameter  $D_a$  of as small as about 36.5 mm.

The pitch enlarging position is such a position back from the end 124 (125) by  $90^\circ$  with respect to the spiral axis as viewed from below the spirally-wound glass tube 120.  
20 Between the turning unit 121 to the pitch enlarging position, the spirally-wound glass tube 120 has a pitch  $P_{2t}$  of 20 mm and a pitch  $P_{1t}$  of 10 mm. The pitch  $P_{2t}$  is a pitch of parts of the spiral unit 122 adjacent in the spiral-axis direction or a pitch of parts of the spiral unit 123 adjacent in the  
25 spiral-axis direction (vertical direction in FIG. 3). The

pitch  $P_{1t}$  is a pitch of a part of the spiral unit 122 and a part of the spiral unit 123 adjacent in the spiral-axis direction.

Accordingly, a minimum gap between glass tube parts adjacent in the direction parallel to the spiral axis A is about 1 mm. It is preferable that this gap is 3 mm or smaller. This is due to the following reason. When the gap is larger than 3 mm, the total length of the arc tube 110 is inevitably long, and also, adjacent glass tube parts are so apart from one another that the problem of uneven illuminance occurs.

The spiral angle  $\alpha$  employed between the turning unit 121 to the pitch enlarging position is about  $76.7^\circ$ . The spiral angle  $\beta$  employed between the pitch enlarging position and the ends 124 and 125 is about  $69.2^\circ$ .

The distance between the electrodes 130 (between the filament coils 131) within the arc tube 110 is 400 mm. The total length of the arc tube 110 (the distance from the tip of the projected part 126 of the arc tube 110 to its bottom end where the electrodes are sealed in the direction parallel to the spiral axis A) is 62.8 mm.

The circumferential wall 220 of the holding member 210 has an outer diameter of 38.5 mm and a height of about 14.6 mm.

On the other hand, in a state where the glass tube 120 with the above-described construction is held by the holding

member 210, the minimum distance L1 between the filament coil 131 within the glass tube 120 and the edge of the insertion opening 231 (232) is 6 mm. Also, the electrodes 130 are sealed in the glass tube 120 in a state where the filament coils 5 131 are inserted into the glass tube 120 to such positions away from the ends of the glass tube 120 by about 14 mm.

It should be noted here that although the present invention is applied to the compact self-ballasted fluorescent lamp corresponding to a 60W incandescent lamp, the present invention may be applied to compact self-ballasted fluorescent lamps corresponding to incandescent lamps with other wattages. In this case, the dimensions of the arc tube, the total length of the compact self-ballasted fluorescent lamp, the type of the base, etc., are different from those described in the 15 above embodiment.

### 3. Rising Characteristics

#### (a) Rising Characteristics Test

A test to examine rising characteristics at the lighting startup was conducted on the compact self-ballasted fluorescent lamp 100 with the above-described construction. 20 The compact self-ballasted fluorescent lamp 100 with the above-described construction is hereafter referred to as the "present invention", and the compact self-ballasted fluorescent lamp described in the Related Art is referred to as the "conventional lamp" to differentiate it from the "present 25

invention".

As described in the Problems to be Resolved by the Invention, the present invention was lit after the total lighting time of 100 hours and 6000 hours. The relationship  
5 between (a) a luminous flux value relative to a luminous flux value during the steady lighting state and (b) an elapsed lighting time was examined. It should be noted here that in this test the lamps were lit with its base being oriented upward.

10 As shown in the figure, the rising characteristics of the present invention are such that the time required by the relative luminous flux value to reach 60% is about 7.5 seconds for the total lighting time of 100 hours (the same as that for the conventional lamp), but is about 9 seconds for the  
15 total lighting time of 6000 hours.

Comparing the present invention and the conventional lamp in terms of the time required by the relative luminous flux value to reach 60% after the total lighting time of 6000 hours, the time is 20.5 seconds for the conventional lamp  
20 and 9.5 seconds for the present invention, implying that the present invention shows a great improvement.

#### (b) Amount of Mercury in the Glass Tube

For the present invention, an analysis of component was conducted at positions, in the vicinity of the filament  
25 coil 131, on the inner surface of the glass tube 120 after

the total lighting time of 6000 hours. The analytical result indicates that 20 to 30% of mercury enclosed in the arc tube 120 sputtered and evaporated from the filament coil 131, and reacted with an electron emissive material adhered to the inner surface of the glass tube 120 to form one type of amalgam (molecular absorption spectrometry was used for the analysis).

For the conventional lamp, too, the same analysis was conducted at positions, in the vicinity of the filament coil 131, on the inner surface of the glass tube 120 after the total lighting time of 6000 hours. The analytical result indicates that 50 to 70% of mercury enclosed in the arc tube sputtered and evaporated from the filament coil, and reacted with an electron emissive material adhered to the inner surface of the glass tube to form one type of amalgam.

#### (c) Conclusions

For the present invention after the total lighting time of 6000 hours, mercury enclosed in the glass tube is reduced by a smaller amount, and also better rising characteristics are obtained as compared with the conventional lamp. Due to this, the rising characteristics are considered to be affected by an amount of mercury present within the glass tube.

The following describes the reasons why the present invention can better suppress a reduction in the amount of mercury than the conventional lamp.

An electron emissive material applied to the filament

coil usually sputters and evaporates due to lighting, and is adhered to the inner surface of the glass tube (this adhered material is hereafter referred to as "blackened material"). The position on the inner surface of the glass tube 120 to which the blackened material is adhered is within the holding member 210 for the present invention, whereas the position is outside the holding member for the conventional lamp.

During the OFF time, the temperature in the vicinity of the blackened material adhered to the inner surface of the glass tube is higher for the present invention than for the conventional lamp. Further, the temperature at the inner surface of the glass tube is lowered less for the present invention than for the conventional lamp. Accordingly, the temperature of the blackened material adhered to the inner surface of the glass tube 120 is higher for the present invention than for the conventional lamp.

On the other hand, mercury has a property of gathering toward lower-temperature positions. It is considered that, even after the compact self-ballasted fluorescent lamp is made OFF, the temperature of the blackened material remains high for the present invention, and mercury within the glass tube does not gather around the blackened material, and therefore, the reaction between the blackened material and mercury is suppressed.

For the present invention, therefore, the amount of

mercury consumed within the glass tube along with longer hours of the total lighting time can be reduced. Due to this, the rising characteristics at the initial use of the lamp can be maintained at a high rate, and the rising characteristics after the lighting time of long hours can be greatly improved.

#### 4. Other Matters

##### (a) Position of the Filament Coil

Although the above embodiment describes the case where the minimum distance L1 between the filament coil and the edge of the insertion opening is 6 mm, the minimum distance L1 may be in a range of 0 to 10 mm inclusive.

This range is determined due to the following reason. When the minimum distance L1 is smaller than 0 mm (where the filament coil is positioned outside the holding member), the effect of improving the rising characteristics at the lighting startup after the total lighting time of long hours cannot be sufficiently obtained. When the minimum distance L1 is larger than 10 mm, the luminous flux produced by the arc tube is reduced by more than 5% of the luminous flux of the compact self-ballasted fluorescent lamp in which the filament coil is positioned outside the holding member. This is not preferable in view of maintaining the quality of the lamp.

##### (b) Amount of Mercury Enclosed in the Arc Tube

The inventors of the present application first attributed the degradation of the rising characteristics at

the lighting startup after the total lighting time of long hours, to the reduction in the amount of mercury caused by the reaction between the blackened material adhered to the inner surface of the glass tube and mercury.

5           The inventors then conducted the same rising characteristics test on the conventional lamp (in which the filament coil is positioned outside the holding member) by increasing an amount of mercury enclosed within the glass tube to 8 mg. As a result, the rising characteristics at the  
10 lighting startup were not degraded after the total lighting of long hours. However, the blackened material was adhered, in the vicinity of the filament coil, to the inner surface of the glass tube, and an amalgam was formed there.

          It seems that the problem can be solved by adding an  
15 amount of mercury to be reacted with the blacked material adhered to the inner surface of the glass tube, to the amount of mercury to be enclosed in the glass tube. In view of environmental protection, however, the recent trend is to reduce the amount of mercury, which is a toxic substance,  
20 enclosed in the glass tube. The present invention can effectively suppress consumption of mercury within the glass tube by holding the arc tube in a state where the filament coil is positioned within the holding member, and can provide an effective means of reducing the amount of mercury to be  
25 enclosed.



Although the above embodiment describes the case where  
3 mg of mercury is enclosed in the glass tube, the amount  
of mercury to be enclosed may be in a range of 2 to 5 mg.  
This range is determined due to the following reason. When  
5 the enclosed amount of mercury is smaller than 2 mg, a sufficient  
amount of mercury does not present in the glass tube. Also,  
even when the enclosed amount of mercury is larger than 5  
mg, an amount of mercury present in the glass tube at the  
lighting is substantially the same as when the enclosed amount  
10 is 5 mg or smaller, due to the mercury vapor pressure within  
the glass tube.

#### <Modifications>

Although the present invention is described based on  
the above embodiment, the contents of the present invention  
15 should not be limited to specific examples shown in the above  
embodiment. For example, the following modifications are  
possible.

#### 1. Compact Self-Ballasted Fluorescent Lamp

It is known that an electron emissive material on a  
20 filament coil evaporates due to lighting, and is adhered to  
the inner surface of the glass tube in the vicinity of the  
filament coil. Mercury within the arc tube reacts with the  
blackened material (electron emissive material) adhered to  
the inner surface, regardless of for example whether a main  
25 amalgam or an auxiliary amalgam is provided or not, and whether

a globe covering the arc tube is provided or not. Accordingly, the present invention is applicable to a compact self-ballasted fluorescent lamp in which a main amalgam and an auxiliary amalgam are provided in its glass tube, and further  
5 to a compact self-ballasted fluorescent lamp that does not include a globe covering its arc tube.

When the present invention is applied to a compact self-ballasted fluorescent lamp including a main (and/or auxiliary) amalgam in its glass tube, mercury present within  
10 the glass tube 120 returns to the amalgam without approaching to a blackened material when the lamp is made OFF, even after the total lighting time of long hours. Therefore, the rising characteristics of this compact self-ballasted fluorescent lamp are not degraded so much. In this sense, such an  
15 advantageous effect described in the above embodiment may not be produced in the case of this lamp.

## 2. Dimensions of the Arc Tube

Although the above embodiment describes the case where the arc tube has a double-spiral shape formed by a glass tube  
20 wound from its middle to both ends around one axis, the arc tube may have another shape.

For example, the arc tube may have a "4U construction" in which four U-shaped glass tubes are combined together as shown in FIG. 8A. The following briefly describes a compact  
25 self-ballasted fluorescent lamp 501 including an arc tube

502 having the 4U construction, with reference to FIGS. 8A and 8B.

The glass tube 509 has the above-described U shape, and is composed of a pair of straight parts 509a and a bent part 509b joining one ends of the straight tube parts 509a. The arc tube 502 is formed by placing the four glass tubes 509 in a substantially square shape so that the glass tubes 509 surround the central axis of an axial case 503 as their substantially center as viewed in the direction of the central axis of the axial case 503, and bridge-connecting adjacent ones of the other ends of the straight parts 509a except one pair. At the other end of the one pair of straight parts 509c, electrodes 530 that are the same as the electrodes described in the above embodiment are sealed.

The holding member 504 is a flat plate member, and has eight insertion openings 504a through which the other ends of the straight parts 509a of the glass tubes 509 constituting the arc tube 502 are inserted. The holding member 504 has, a holding cylinder 504b surrounding each insertion opening 504a for holding the straight parts 509a of the glass tubes 509.

The holding member 504 has substrate engagement hooks to be engaged with a substrate 541 on which an electronic ballast 540 is mounted, and case engagement hooks 504c to be engaged at the inner surface of a case 503. The method

of attaching the holding member 504 to the substrate or to the case should not be limited to such a engagement method, but may for example be a method using screws.

As shown in FIG. 8B, for the arc tube 502, the filament  
5 coil 531 within the glass tube 509 is positioned at the side of the holding member 504 where the case 503 is positioned. The minimum distance L2 between the filament coil 531 and the edge of the insertion opening 504a in the insertion direction E of the glass tube 509 inserted through the insertion  
10 opening 504a is in a range of 0 to 10 mm inclusive.

The minimum distance L2 is a distance between a plane F3 and a plane F4 in the insertion direction E. The plane F3 is a plane that includes positions on the filament coil 531 that are supported by the lead wires 532 and 533, and  
15 that is perpendicular to the tubular axis C2 of the glass tube 509. The plane F4 is a plane that includes positions, closest to the filament coil 531 in the insertion direction E, on the boundary at which the glass tube 509 enters in the holding member 504 (the holding cylinder 504b), and that is  
20 perpendicular to the tubular axis C2.

As in the above embodiment, the degradation of the rising characteristics which occurs to the conventional lamp after the total lighting time of long hours does not occur to the compact self-ballasted fluorescent lamp 501 with this  
25 construction.

### 3. Main Amalgam

For the lamp of the present invention, the inner diameter of the glass tube may be at any value in a range of 5 to 9 mm. By connecting the top part of the arc tube (the bent part of the glass tube) to the globe via silicone resin, and setting the inner diameter of the glass tube in this range, the temperature of the arc tube during lighting can be made substantially the same as such a temperature that enables the luminous flux produced by the arc tube to be substantially the maximum. Therefore, a high luminous efficiency can be obtained even without utilizing a main amalgam. Further, because the lamp of the present invention does not use a main amalgam, the rising characteristics during lighting can be made similar to the rising characteristics of typical fluorescent lamps.

### 4. Electrodes

Although the above embodiment describes the case where the electrodes having such a construction where the filament coil is supported using the bead glass mount method are used, electrodes using other methods, e.g., a stem method, may instead be used.

### 5. Holding Member

The above embodiment describes the case where the holding member has, on its end wall, a pair of tube-holding structures each including the insertion opening, the guide unit, and

the cover unit. Although it is preferable that the tube-holding structure includes all of the insertion opening, the guide unit, and the cover unit, the tube-holding structure may not include, for example, the guide unit. In this case, an opening is to be formed instead of the guide unit, to serve as the insertion opening. Alternatively, the tube-holding structure may not include the cover unit. In this case, an opening is to be formed instead of the cover unit, to serve as the insertion opening.

#### 6. Fluorescent Lamp

Although the above embodiment describes the case where the present invention is applied to a compact self-ballasted fluorescent lamp, the present invention can be applied for example to a fluorescent lamp shown in FIG. 9.

This fluorescent lamp 600 includes a double-spiral arc tube 610 formed by a glass tube 620 spirally wound to its ends, a cylindrical holding member 630 having a closed bottom and holding the arc tube 610 (the end-vicinity parts of the glass tube 620), a case 640 fit to cover the circumferential wall of the holding member 630, a globe 650 covering the arc tube 610, and a single base 660 (e.g., GX10q type) to be fit in a socket of a lighting fixture and receiving power supply.

The fluorescent lamp 600 differs from the above compact self-ballasted fluorescent lamps 100 and 501 in that an electronic ballast is not contained in the holding member

630 and the case 640, and in that the base 660 is not a screw-type base used also for incandescent lamps.

(a) Dimensions of the Arc Tube

The above embodiment describes the case where the present  
5 invention is applied to a compact self-ballasted fluorescent lamp alternative to an incandescent lamp. Therefore, the compact self-ballasted fluorescent lamp is described to have the above dimensions, in particular, the annular outer diameter of the double-spiral shape being 40 mm or smaller,  
10 down to about 30 mm. When the present embodiment is applied to the above fluorescent lamp, however, the above limitations on the dimensions of the arc tube can be removed. As one example, the annular outer diameter of the arc tube may be larger than 40 mm.

15 The spiral angle  $\alpha$  employed between the middle of the glass tube and the pitch enlarging position and the spiral angle  $\beta$  employed between the pitch enlarging position to the ends are determined depending on the targeted annular outer diameter and spiral pitch of the arc tube. If, for example,  
20 the targeted annular diameter of the arc tube is increased, the spiral angles  $\alpha$  and  $\beta$  are changed accordingly.

7. Holder

The holding member relating to the above embodiment holds the arc tube by bonding the ends of the glass tube to the  
25 inner surface of the holder via silicone resin. The ends of

the glass tube are inserted in the holding member through the insertion openings formed in the end wall of the holding member. Also, for the compact self-ballasted fluorescent lamp relating to the modification 2 and the fluorescent lamp  
5 relating to the modification 5, too, the holding member having the same construction as that described in the above embodiment is used to hold the arc tube.

On the other hand, the holder of the present invention holds the arc tube by fixing the glass tube inserted through  
10 the insertion openings. In the above embodiment and the modifications, the holder is composed of the holding member and the case.

Accordingly, the construction of the holder of the present invention should not be limited to the construction  
15 described in the above embodiment and the modifications. For example, the holder may be such that the large-diameter part of the case is fit at the inner surface of the circumferential wall of the holding member. Further, separate members may be provided as a member where the insertion openings are formed  
20 and a member for fixing the glass tube. To be more specific, a plate member in which the insertion openings are formed and a cylindrical member to which the ends of the glass tube are fixed may be provided separately, and these separate members may be individually attached to the case.

25 8. Globe



Although the compact self-ballasted fluorescent lamps 100 and 501 relating to the above embodiment and the modification 2 and the fluorescent lamp 600 relating to the modification 5 respectively include the globes 400, 506, and 5 650 covering the arc tubes 110, 502, and 610, the present invention can be applied to a compact self-ballasted fluorescent lamp without a globe, or to a fluorescent lamp without a globe.

For the compact self-ballasted fluorescent lamp without 10 a globe or the fluorescent lamp without a globe, heat generated during lighting is directly released from the arc tube. By setting the tube inner diameter of the glass tube in a range of 5 to 9 mm inclusive, the temperature of the arc tube during lighting becomes substantially the same as such a temperature 15 that enables the luminous flux produced by the arc tube to be substantially the maximum.

Although the present invention has been fully described by way of examples with reference to the accompanying drawings, it is to be noted that various changes and modifications will 20 be apparent to those skilled in the art. Therefore, unless such changes and modifications depart from the scope of the present invention, they should be construed as being included therein.